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# Effect of coal fly ash treatments on synthesis of high-quality zeolite A as a potential additive for warm mix asphalt



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# HIGHLIGHTS

# G R A P H I C A L A B S T R A C T

- High-quality zeolite A is successfully obtained from fly ash.
- Fly ash is subjected to different treatments prior to zeolite syntheses.
- A novel pore characterization method based on CO<sub>2</sub> isotherms and molecular simulation is applied.
- The obtained zeolite acts decreasing the work temperature of mix asphalt.

# ARTICLE INFO

Keywords: Zeolite A Microporous material Fly ash Warm mix asphalt Industrial waste



# ABSTRACT

An experimental investigation on the synthesis of zeolite A, based on the treatment of fly ash and controlled extraction of silica and alumina from coal fly ash, combined with the adjustment of the reaction mixtures aiming minimum amount of secondary phases, is presented herein. The precursor samples of fly ash and the obtained zeolites were widely characterized considering different techniques including powder X-ray diffraction, infrared vibrational spectroscopy, scanning electron microscopy, and thermogravimetric analysis. A new pore characterization technique that combines experimental CO<sub>2</sub> isotherms at 273 K and molecular simulation was specially developed for this system. The synthesized zeolites presented zeolite A as the major phase, with high crystallinity and low degree of defects in the supercages. The treated fly ashes affected the synthesis yield and the properties of the obtained zeolites, which proved to be efficient in decreasing the viscosity of the modified asphalt cement, during heating, contributing to improve its workability.

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# 1. Introduction

Coal is the world's most abundant fossil fuel, with reserves of approximately one trillion tons [1], making coal combustion an important process for generating electricity in many countries [2]. When burned in thermal power plants, it generates residues in form of tiny particles which are carried by the combustion gases. Such residues are called fly ashes and are collected by filter systems. Fly ashes are thin particles in powder form, with a predominately spherical shape, either compact or hollow, with maximum diameter of 75  $\mu m$  and blackish coloration which varies depending on its composition. Their chemical composition is mainly silica (SiO<sub>2</sub>), alumina (Al<sub>2</sub>O<sub>3</sub>), iron oxide (Fe<sub>2</sub>O<sub>3</sub>), and calcium oxide (CaO) [3]. The dominant mineral phases that compose fly ashes are quartz, kaolinite and ilite, while less predominant phases such as calcite, pyrite and hematite can also be found [4]. Fly ashes are classified into two groups, depending on the combination of SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, and Fe<sub>2</sub>O<sub>3</sub>. Fly ash containing more than 70% of these three compounds is classified as F type, while a concentration in the range 50-70% implicates in a fly ash type C, in which concentration of CaO tends to be higher [5,6].

As a solid residue, fly ash is discarded in open pit deposits and, given its ease of leaching by water, metals such as cadmium, cobalt, chromium, nickel, and lead can be released, strongly impacting the environment [7,8]. Therefore, fly ash accumulation represents a serious environmental problem which needs thorough consideration. In fact, there are numerous studies demonstrating its potential for other purposes [9], including the synthesis of zeolites [10,11].

Zeolites comprise a class of porous aluminosilicates with crystalline structure. Their structure can be summarized as a combination of tetrahedral  $[SiO_4]^{4-}$  and  $[AIO_4]^{5-}$  joined by oxygen atoms [12]. Their chemical composition is commonly represented by:

$$A_{y/m}^{m+} \left| (SiO_2)_x \left( AlO_2^{2-} \right)_y \right| \cdot zH_2O$$

where A is a cation with charge m, (x + y) is the number of tetrahedra per crystallographic unit cell, and x:y is the silicon:aluminum ratio that, based on the Löwenstein's rule, cannot be higher than 1, and therefore the Al–O–Al linkages are not allowed [13].

Properties as high ion exchange capacity, high surface area, and high chemical stability, make zeolites suitable materials to be employed in innumerous applications such as adsorption in gas purification, ion exchanger in builders, catalysis in oil refining, petrochemistry and biotechnology [14]. Zeolites can be synthesized via many different routes and from different sources. The hydrothermal method is the most common route and involves the treatment of the reagents in strong alkaline medium, together with heating in a closed system. In some cases, ultrasound and microwave radiation can be used as more effective energy sources [15,16]. The raw materials used include silica and aluminum sources such as sodium aluminate and silicate salts, colloidal silica, aerosol silica, as well as other materials as clays [17] and fly ash [18,19]. In fact, the first investigations of zeolite synthesis from fly ash were based on its similarity with volcanic material, a precursor of natural zeolite [20,21].

Nevertheless, synthesizing zeolites from fly ash is not a straightforward task, since high temperatures (90–225 °C) and prolonged synthesis times (24–72 h) are required [22]. Two activation methods are usually applied. In the first one, alkaline fusion takes place at high temperatures, followed by hydrothermal treatment. The second method is the direct hydrothermal, in which the fusion step is omitted. In any case, obtaining the zeolite involves a series of variables such as the type and concentration of the alkali solution used, solution/solid ratio, aging time, mixture techniques, pressure during crystallization, and heating sources [23]. Several works report the synthesis of zeolites as mixtures of phases, as zeolites X, P, Q and S [24], A and T [25]. Musyoka et al. reported the synthesis of zeolite A [26] and X [27] by means of fly ash alkali fusion at 550 °C, followed either by hydrothermal reaction under autogenous pressure in closed system or by reaction using ultrasound. A combination of methods resulted in synthesis of zeolites A and P by activating ashes with concentrated sodium hydroxide solution and adjusting the silicon/aluminum ratio by dissolving metallic aluminum [28]. The main difficulties faced in zeolite synthesis from fly ash are related to the crystallization of secondary phases.

Within their pore structures, zeolites retain considerable amounts of water, which can be released by heating. Zeolite type A in particular can retain approximately 20 wt% of water, being therefore a potential additive in the preparation of warm mix asphalt (WMA). Water-containing technologies promotes the micro-foaming of the asphalt binder, which causes a better coating of the aggregate at lower temperatures than conventional ones [29]. As a consequence of water being released from zeolite, a typical zeolite/WMA can be manufactured at temperatures 20–40 °C lower than an equivalent hot mix asphalt (HMA). Additionally, warm mixtures are presented as an alternative to reduce the emission of CO<sub>2</sub> and polluting gases, as well as to reduce energy consumption, contributing to minimize environmental impacts associated to asphalt preparation. In this context, and considering the complexity in using fly ash for zeolite synthesis, this study investigates the synthesis of zeolite type A from fly ash and its potential as a cost-effective additive for WMA.

# 2. Experimental

# 2.1. Materials

Fly ash (FA) used in this work was provided by the ENEVA-Pecém thermal power plant located at Ceará, Brazil. The ashes were collected from the manga filters and are classified as fly ash class F [30]. Prior to the treatments the FA was ground and sieved ( $<74 \mu$ m). The base Asphalt Cement (AC) with penetration grade 50/70 was provided by Lubnor (Petrobras, Brazil). Table 1 presents the datasheet related to the main properties obtained from the empirical and rotational viscosity tests. Additional information about AC and zeolite modified AC is presented in Table S1.

### 2.2. FA treatments

FA was submitted to three different treatments. The first one consisted of the removal of the magnetic fraction by spreading FA samples between two thin paper sheets and applying Neodymium-based magnet on the paper surface in smooth movements repeated times. The remaining non-magnetic fraction was referred as FA-MT (fly ash-magnetic treated). For the acid treatment, 10.00 g of FA were mixed with 100 mL of HCl 2.0 mol L<sup>-1</sup> and heated at 90 °C for 1 h, under reflux and vigorous magnetic stirring. The remaining solid was washed with deionized water 3 times, dried at 80 °C overnight, and named as FA-AT (acid treated samples). Finally, the last treatment consisted of a combination of magnetic separation and acid treatment (FA-MT/AT).

# 2.3. Zeolite synthesis

For the zeolite synthesis, 10.0 g of each sample, i.e., the untreated one (FA) and those submitted to different treatments (FA-MT, FA-AT and

#### Table 1

Asp	hat	cement	data	for	the	empirical	and	rotational	viscosity	tests.
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Assays	Standards	Results
Empirical tests		
Penetration at 25 °C (dmm)	ASTM D5	58
Softening point (°C)	ASTM D36	48
Brookfield viscosity tests		
135 °C (cP)	ASTM D 4402	394.2
150 °C (cP)	ASTM D 4402	191.7
177 °C (cP)	ASTM D 4402	70.0

Source: Asphalt cement datasheet.

FA-MT/AT), were added to 100 mL of NaOH 4.00 mol  $L^{-1}$ , in a polypropylene flask coupled to a reflux apparatus, and heated to 90 °C under vigorous magnetic stirring for 1 h. The amount of silica and alumina extracted to the solution was determined indirectly by means of X-ray fluorescence analyses of the solid residues. The zeolite syntheses were carried out via hydrothermal route using the NaOH-extracted silica and alumina from the samples FA, FA-MT, FA-AT and FA-MT/AT, as the only silica source and the main aluminum source. In all cases, the following reactional mixture was used:

#### $3.165 \text{ Na}_2\text{O}$ : $Al_2\text{O}_3$ : $1.926 \text{ SiO}_2$ : $128 \text{ H}_2\text{O}$

As the treatments employed affected the amount of aluminum in the fly ash NaOH-extracted solution, the composition of the reaction mixtures was adjusted by using sodium aluminate. NaOH also had to be added to the reaction mixture so that the required concentration could be achieved. Nevertheless, it was observed that part of the iron present in the fly ashes samples precipitates in form of iron hydroxide during the silica and alumina extraction process. This way, the correspondent decreasing in the NaOH concentration had to be balanced, which was accomplished considering the amount of iron present in the solid residues obtained from the alkali extraction.

The precursor synthesis gels were transferred to a Teflon-lined stainless-steel autoclave and heated at 100  $^{\circ}$ C for 4 h under autogenous pressure and static conditions. The obtained solid was washed several times with distilled water until constant pH and dried at 80  $^{\circ}$ C overnight. The zeolites obtained from the different FA samples were named: ZA, ZA-AT, ZA-MT, and ZA-MT/AT.

# 2.4. Characterization

The efficiency of the zeolite synthesis from fly ash is a requirement for a proper assessment of the zeolite effect as an additive for WMA. Therefore, a comprehensive structural, spectroscopic, and morphological study of the synthesized zeolites was carried out. The characterization of precursor samples as well as the synthesized zeolites was conducted by means of X-ray diffractometry, infrared spectroscopy, scanning electron microscopy and cation exchange capacity determination. In molecular sieves with very small access windows such as zeolite A, clinoptilolite and chabazite, the use of either N<sub>2</sub> or Ar for obtaining adsorption/desorption isotherms at low temperatures is not feasible. For this reason, herein we apply a new approach to characterize the pore volume combining data from experimental  $CO_2$  adsorption isotherms at 273 K with molecular simulation.

# 2.4.1. X-ray diffraction (XRD)

Powder XRD patterns for the samples with particle sizes below 74 mm (400 mesh) were collected using a X-ray powder diffractometer Xpert MPD (Panalytical). The X-ray tube (Co) operated at 40 kV and 40 mA. The high-resolution diffraction is obtained with a hybrid monochromator for incidence beam, which consists of mirror and Ge monochromator producing a parallel and highly monochromatic beam, respectively. The data were collected with Pixcel solid-state detector. The XRD measurements were performed by using a 255 channels detector, with step scan of  $0.013^{\circ}$  in 20 angular interval from 5° to 50°.

Structure refinement was performed for the resulting zeolite samples by Rietveld method using GSAS software package with EXPGUI interface [31,32], observing the adjustments between observed and calculated patterns by the  $\chi^2$  parameter. From these results, quantitative analysis was carried out and average crystallite sizes were calculated by means of Scherrer equation [33] using the full-width at half maximum (FWHM) of the diffraction peaks, which was corrected for instrumental broadening (measured through analysis of LaB<sub>6</sub> crystals, SRM 660C).

# 2.4.2. Infrared vibrational spectroscopy

Fourier transform infrared (FTIR) spectra were obtained for samples

prepared in KBr wafers using a Shimadzu IRTracer-100 FTIR spectrometer in the region 4000-400  $\text{cm}^{-1}$  and nominal resolution of 2  $\text{cm}^{-1}$ .

### 2.4.3. Scanning electron microscopy (SEM)

A FEG equipment model Quanta 450 was used with detectors for secondary electrons and energy-dispersive X-ray. Prior to the analyses, samples were prepared on an aluminum support using carbon double-sided sticky tape and coated with a thin gold layer.

# 2.4.4. Cation exchange capacity (CEC)

CEC of all samples were determined by promoting cation exchange with ammonium ion. In short, 1.00 g of each sample was added to 10.0 mL of NH<sub>4</sub><sup>+</sup> 10 wt%, stirred in orbital shake for 8 h, followed by 16 h in static conditions. The solids were collected, washed several times with distilled water, and dried at 60 °C overnight. The quantification of NH<sub>4</sub><sup>+</sup> ions was carried out by thermal decomposition of ammonium to ammonia, which was titrated with H<sub>2</sub>SO<sub>4</sub> 0.01 mol L<sup>-1</sup>. The results were converted to mol kg<sup>-1</sup>.

# 2.4.5. Thermal analysis

Thermal analysis of ZA sample was performed using equipment Netzsch model STA 499 F3 in a temperature range of 25–350 °C with heating rate of 5 °C min<sup>-1</sup> and under nitrogen atmosphere with flow of 50 mL min<sup>-1</sup>. DCS analysis was carried out in equipment Shimadzu DCS-50, in a temperature range of 25–350 °C with heating rate of 5 °C min<sup>-1</sup>.

# 2.4.6. CO<sub>2</sub> adsorption/desorption isotherms and molecular simulation

 $CO_2$  adsorption isotherms were obtained at 273 K in an Autosorb-iQ<sub>3</sub> equipment (Quantachrome, USA) and used to characterize the micropore volume of the studied zeolites. The samples (*ca.* 0.1 g) were previously degassed under the following conditions: heating under high vacuum (10<sup>-4</sup> mbar), from room temperature to 180 °C, at a heating rate of 2 °C min<sup>-1</sup>, maintaining at the final temperature for a period of 6 h.

Molecular simulation was used to determine the pore integrity of the synthesized zeolite samples. A new approach involving the use of local isotherms of a limited number of zeolite supercages/unit cell was applied. The zeolite A model (Si/Al ratio = 1) used, was obtained through the crystal refinement performed by Pluth and Smith [34]. The model consists of 64 atoms at site I, 24 atoms at site II and 8 atoms at site III, resulting in a unit cell of Na<sub>96</sub>Sl<sub>96</sub>Al<sub>96</sub>O<sub>384</sub>. The CO<sub>2</sub> model was taken from Harris and Yung study [35], which fully reproduces the liquid-vapor equilibrium. The system can be properly described by using Lennard-Jones potentials plus Coulomb contributions. Monte Carlo simulation in the grand canonical ensemble was performed to evaluate adsorption isotherms using the force field adapted from the study of Gomes et al. [36].

# 2.5. Mixing and procedures of asphalt cement (AC) modification with zeolite

The sample ZA was chosen for modification of asphalt cement. Although the yield for the sample ZA was found slightly lower than that of the other synthesized zeolites, its adsorption capacity, measured by CO<sub>2</sub> isotherms at 273 K, was the highest, being 10–18% higher compared to the samples ZA-AT, ZA-MT, and ZA-MT/AT. Besides that, its production involves the simplest route, and therefore it is the most cost-effective material. Thus, this sample was chosen for modification of asphalt cement. In a typical procedure, 4.00 g of zeolite ZA was slowly added to 400.00 g of AC, under mechanical stirring (1500 rpm) at 90  $\pm$  5 °C, for 2 h, using mixer IKA, model RW20. The additive content was 1 wt% of the binder, which was chosen based on previous studies [37,38].

# 2.6. The effect of WMA zeolite additive on asphalt cement properties

In this study, different parameters were considered to evaluate the effect of zeolite as additive for WMA technology: a) to verify the water

release from zeolite, a temperature of 90 °C was used [39,40], b) to investigate the AC viscosity over time, either with or without the synthetized zeolite, the temperature was 120 °C, which is normally used to test the viscosity over time for warm mix asphalt, typically 10–20 °C lower than conventional hot mix asphalt (HMA) [41].

# 2.6.1. Rotational viscosity test to evaluate asphalt cement foaming through zeolite addition

The rotational viscosity was determined for both AC and zeolite modified AC (ZA-AC), using a viscosimeter Brookfield model DVII+. The tests were performed at constant temperature ( $120 \,^{\circ}$ C) and the viscosity values were determined over time. The first two values were recorded at 0.5 and 1 min, respectively, and the subsequent ones at intervals of 5 min, to a total of 31 min.

# 3. Results and discussion

In this section, a comprehensive characterization of the fly ash samples, and the synthesized zeolites is presented. A set of different techniques was employed to assess the effectiveness of the synthesis and the potential of the obtained materials for application in warm mix asphalt. 3.1. XRD

Fig. 1a–d shows the powder XRD patterns for the samples of fly ash and the treated fly ash samples. All samples present quartz, hematite, and magnetite as the major components. Mullite appears only in the untreated fly ash sample (Fig. 1a).

The XRD patterns of the synthesized zeolites are presented in Fig. 1e-h. The main results for the Rietveld structural refinement are

# Table 2 Rietveld refinement output. The major phases are indicated in bold.

	1	5 1		
Sample	Phase	Weight/ %	$\chi^2$	Average crystallite size/nm
ZA-MT/ AT	Zeolite A (24901)	100	1.01	102.4
ZA-MT	Zeolite A (24901)	100	1.02	133.8
ZA-AT	Zeolite A (24901)	95.5	1.14	77.1
	Zeolite Y (201472)	1.8		14.7
	Zeolite RUB-3	0.6		75.0
	(86547)			
	Quartz (26430)	2.1		217.0
ZA	Zeolite A (24901)	96.4	0.93	87.3
	Zeolite ZK-14	3.6		42.5
	(201587)			

ICSD-Inorganic Crystal Structure Database.



Fig. 1. XRD patterns of fly-ash (a) without treatment (FA), and with treatment (b) FA-MT, (c) FA-AT, and (d) FA-MT/AT; XRD patterns of synthesized zeolites (e) ZA, (f) ZA-AT, (g) ZA-MT, and (h) ZA-MT/AT.

summarized in Table 2 and in Fig. S1. The closer the value of  $\chi^2$  to 1.0, the better the adjustment. The results of  $\chi^2$  showed in Table 2 indicate, therefore, that the refinement is reliable.

In all the synthesized zeolite samples (Fig. 1e-h), zeolite A (ICSD 24901) [42] is found as the major crystalline phase, with the correspondent peaks well defined and presenting high intensity. Samples ZA (Fig. 1e) and ZA-AT (Fig. 1f) presented secondary phases in small amounts, while the samples ZA-MT (Fig. 1g) and ZA-MT/AT (Fig. 1h), obtained from the fly ash samples subjected to magnetic separation and to the combination of magnetic separation with acid treatment, respectively, were composed of pure zeolite A phase. The absence of secondary phases in the synthesized samples lead to bigger zeolite crystallite, indicating that in an environment without competition, the zeolite tends to grow more easily. The sample ZA-MT/AT (Fig. 2h) presents peaks at 8.55°  $2\theta$  (200) and 12.04°  $2\theta$  (220) with relative intensity opposite to what is observed in the other samples. This is commonly associated to preferred orientation and may be related to the distribution of occupancy of specific T-sites by Al or even Fe atoms. The acid treatment of the fly ash promotes the removal of iron, what would potentially affect the zeolite crystallization. However, this treatment also removes aluminum from the fly ash, affecting the Si/Al ratios of the reactional mixtures and consequently the Si/Al ratio in the zeolites, which is a well-known parameter that strongly influences the chemical functionality of zeolites [43].

# 3.2. Chemical composition and cation exchange capacity

The amount of Si, Al, and Fe, as well as CEC values, for all the samples, are shown in Table 3. For comparison purposes, a sample of zeolite A (A) synthesized via the classical method, employing sodium metasilicate and sodium aluminate, is also included. It is possible to observe that the Si/Al ratio varies depending on the treatment applied to the ashes. The CEC values determined for the zeolite samples varied from 1.53 to 2.26 mol kg<sup>-1</sup>, which are considerably higher than the values verified for the precursor samples and slightly higher than that observed for the reference zeolite (sample A). These numbers are compatible with results from other works [44–46]. Furthermore, it is also important to highlight that the sample ZA-MT/AT showed the highest CEC value, reinforcing the effectiveness of the fly ash combined treatment for the synthesis of zeolite with improved properties.

# Table 3

Chemical composition, determined by EDS, and cation exchange capacity (CEC), determined by Kjeldahl method, of the fly ash and the synthesized zeolite samples.

Sample	Si/%	Al/%	Fe/%	Si/Al	CEC/mol kg <sup>-1</sup>
А	19.9	17.9	0.0	1.069	1.267
FA	27.18	14.25	6.46	1.831	0.1461
ZA	18.66	18.89	0.82	0.947	2.142
FA-MT	32.97	15.52	10.22	2.038	0.1614
ZA-MT	22.10	21.34	0.25	0.995	1.535
FA-AT	34.42	10.94	4.13	3.027	0.3332
ZA-AT	23.37	21.43	0.0	1.061	1.665
FA-MT/AT	34.13	11.38	6.09	2.886	0.1952
ZA-MT/AT	19.97	20.32	0.0	0.944	2.261

# 3.3. FTIR

As vibrational spectroscopy in the infrared region provides important information related to specific chemical bonds, it is helpful for evaluating the influence of the treatments applied to the fly ashes and the structural changes associated to the synthesized zeolites. FTIR spectra of the fly ash samples are presented in Fig. 2a–d. Three main signals are observed: the large band centered at 1085 cm<sup>-1</sup>, which can be associated with the presence of aluminosilicates with some amorphous nature, the band at 470 cm<sup>-1</sup> related to O–Si–O bending vibrations, and the band at 788 cm<sup>-1</sup>, characteristic of O–Si–O symmetric stretching vibration [47]. No substantial changes were observed for the fly ash samples after the treatments (Fig. 2b–d), except for some slightly improvement in the resolution of the large band at 1085 cm<sup>-1</sup> for the samples FA-MT and FA-MT/AT, what can be associated to elimination of Fe-rich particles present in the FA.

The spectra of the synthesized zeolites are shown in Fig. 2e–h. Compared to the fly ash samples spectra (Fig. 2a–d), several new bands can be observed, clearly indicating tranformation of their structures. The region between 700 and 400 cm<sup>-1</sup> is known as the fingerprint zone, due to specific vibrational modes related to the zeolite structure. For the synthesized zeolites, it is possible to observe three bands in this region. The band centered at 462 cm<sup>-1</sup> is characteristic of internal vibration of Si (Al)–O bending, while the band at 557 cm<sup>-1</sup> is due internal vibration of double-four rings. The strong signal at 1002 cm<sup>-1</sup> can be associated to Si (Al)–O asymmetric stretching [48,49]. The large band at 3450 cm<sup>-1</sup> and the well defined band at 1648 cm<sup>-1</sup> are related to the presence of structural water in the zeolites.



Fig. 2. FTIR spectra of fly-ash samples: (a) with no treatment, (b) with acid treatment, (c) with magnetic treatment. and (d) with combined magnetic and acid treatments; FTIR spectra of synthesized zeolites (e) ZA, (f) ZA-AT, (g) ZA-MT, and (h) ZA-MT/AT.

#### 3.4. SEM

SEM is a valuable technique for morphology and surface texture studies of the individual particles. The SEM images for the fly ash samples, presented in Fig. 3, show uniform spherical particles, supposedly hollow, commonly referred to as cenospheres. These particles are formed during the expansion of the gases produced in the burning of the coal. It is possible to visualize a smoothing over the particle surfaces after the acid treatment (Fig. 3c–d and g-h), what might be the result of the acid attack to the iron oxides compounds deposited on these particles [50,51].

Particle morphology is usually an important factor for the final properties of several materials. Surface features of zeolite A may vary substantially [52,53], and as the zeolite morphology affects directly its applications [54], it is crucial to understand how the treatments applied to the fly ash samples affects the morphology of the synthesized zeolites. SEM images of the synthesized zeolites are presented in Fig. 4.

In all the samples, the characteristic cubic crystal of zeolite A is observed, with apparent homogeneous size distribution. Sample ZA (Fig. 4a and b) shows well-defined sharp edges, while all the other samples present chamfered edges (Fig. 4c–h). This difference in the crystal habits may be associated with many variables. Nevertheless, the reaction mixture composition is believed to be the major responsible for changes in the crystal morphologies. Results from early studies have indicated that the nature of the aluminum source plays a central role in zeolite A morphology [55]. In general, its organic form favors zeolite crystals with chamfered edges, possibly by influencing the water activity in the gel synthesis. As shown in Table 3, the FA sample possesses 14.25 wt% of aluminum, but its concentration is reduced to 10.94 wt% and 11.38 wt% with acid treatment, in sample FA-AT, and with the combined magnetic/acid treatment, respectively.

#### 3.5. CO<sub>2</sub> adsorption/desorption and molecular simulation

 $N_{\rm 2}$  (at 77 K) and Ar (at 87 K) are the most accepted molecules used as probes for textural characterization of porous materials. However, due to a pronounced molecular sieved effect accompanied by packing limitations, at low temperatures the rate of diffusion of  $N_2$  and Ar into the microporous system of zeolite A is extremely slow, particularly in the sodic form of this zeolite, which limits the physisorption capacity for these gases [56].

Some studies suggest the use of  $CO_2$  isotherms at 273 K as an alternative strategy for the characterization of materials in which the pores are inaccessible to N<sub>2</sub> and Ar, at cryogenic temperatures [57]. However, due to the strong  $CO_2$ – $CO_2$  interaction and the lack of a proper theoretical background, characterization methods such as BET, BJH and phenomenological approaches based on  $CO_2$  isotherms can be misleading. Furthermore, even the most recent commercial analyzers provide no kernels that allow the application of NLDFT or QSDFT for interpretation of the  $CO_2$  adsorption isotherm on zeolites in terms of pore space. Therefore, a new approach based on molecular simulation has been developed to allow the characterization of the zeolite pore space using adsorption isotherms of  $CO_2$ . For the specific case of zeolite A samples, the first step was to define a standard  $CO_2$  experimental isotherm. The detailed high-resolution  $CO_2$  isotherms obtained by Palomino et al. [58] (Fig. 5a). at 303 K was chosen for this study.

After that, a force field has been established to reproduce the standard experimental isotherm. The isotherm called SC8 (blue line in Fig. 5a) was simulated using the specified force field, being able to reproduce satisfactorily the experimental isotherm. The force field was set by optimizing the match between simulated and experimental isotherms of the pressure value in the inflection point. With a validated force field, it is possible to reproduce the isotherms under different conditions of pressure and temperature and, more importantly, to verify the influence of each supercage cavity in the experimental isotherms.

The experimental CO<sub>2</sub> adsorption isotherms for the samples synthesized in this study are shown in Fig. 5b. Sample ZA adsorbs 10% more than ZA-MT and ZA-MT/AT samples and 18% more than ZA-AT sample. The IUPAC classification of isotherms is the same for all samples (Type I). The details of the adsorption regime at lower pressures shown in Fig. 5b indicate that all isotherms are consistent with the Si/Al ratio equal to 1 and the decrease in CO2 adsorption capacity must be related to defects in the supercages. During synthesis, in the stages of nucleation and crystal growth, several classes of defects may be present. These defects are difficult to identify due to the wide variety of chemical species in the mixture and the lack of knowledge of the nature and structure of precursor species. It has been observed that flaws in the structure of zeolite A can be translated as a proportional decrease in the adsorption capacity caused by the non-functionality of a given number of supercage units. Hence, the developed force field has been used to calculate isotherms for a decreasing number of viable supercages. Zeolite A unit cell has 8 supercages viable for adsorption (Fig. 5c).



Fig. 3. SEM images of the fly-ash samples (a–b) FA (fly-ash without treatment), and the treated samples (c–d) FA-AT (acid treatment), (e–f) FA-MT (magnetic treatment) and (g–h) FA-MT/AT (combined magnetic and acid treatments).



Fig. 4. SEM images of synthesized zeolites (a-b) ZA, (c-d) ZA-AT, (e-f) ZA-MT and (g-h) ZA-MT/AT.



**Fig. 5.** (a) Standard experimental isotherm (squares) of CO<sub>2</sub> (303 K) for zeolite A and simulated isotherm (line) from the appropriate force field. The SC8 label denotes the number of viable supercages per unit cell (8 supercages/unit cell). (b) Experimental and simulated isotherms of CO<sub>2</sub> for zeolite A at 273 K. Experimental isotherms: ZA (circle), ZA-MT (diamond), ZA-MT/AT (green triangle) and ZA-AT (red triangle). Simulated isotherms: SC8 (gray line), SC7 (black line), SC6 (blue line) and SC6 (red line), the numbers 8, 7, 6 e 5 indicate the viable supercages per unit cell. (c) Framework of a zeolite A unit cell. Each unit cell has 8 supercages. Yellow sphere – pore volume of the supercage. Small spheres – cations. Pink – Al, Yellow – Si and Red – O. (For interpretation of the references to color in this figure legend, the reader is referred to the Web version of this article.)

From the zeolite A structure with all 8 functional supercages, simulations have been made with a decreasing number of functional supercages: 7, 6 and 5 (i.e., inactivation of 1, 2 and 3 supercages per unit cell, respectively). The simulated  $CO_2$  adsorption isotherms are

presented in Fig. 5b, together with the experimental data. The gray line (SC8) is the result of the simulated  $CO_2$  adsorption isotherm in a sample without defects, where all supercages are functional. The black (SC7), blue (SC6) and red (SC5) lines are simulated isotherms for theoretical

samples with 7, 6 and 5 viable supercages per unit cell, respectively. The comparison between simulated and experimental isotherms provides interesting conclusions. The ZA sample, with the best performance, appears to have only one defective supercage/unit cell. Considering that an alternative raw material such as fly ash has been used, the synthesis of the ZA sample is an excellent outcome of this study. The structures of ZA-MT and ZA-MT/AT samples are compatible with an average deactivation close to 2 supercages/unit cell and the structure of the worst performing sample, ZA-AT, corresponds to a deactivation of almost 3 supercage/unit cell.

The employed novel characterization approach allows not only the verification of the adsorption capacity of the synthesized samples but also indicates the level of impairment of the porous structure in terms of supercage deactivation.

#### 3.6. Thermal analysis

The role played by zeolite in the warm mix asphalt results from its ability to retain water within its pores and release it at specific temperatures. Thermogravimetric analysis (TGA) and differential scanning calorimetry (DSC) results for zeolite ZA are presented in Fig. 6.

According to the general chemical formula for the unit cell of zeolite A, approximately 22% of its mass corresponds to water. As indicated by TGA, up to 350 °C there is a loss of 17% of mass, which is related to water release. DSC shows distinct thermal events, indicating that water is present in different sites within the zeolite structure. The mass loss around 100 °C refers to adsorbed water, while the loss at higher temperatures (above 200 °C) can be related to dehydration, involving the formation of hydrate complexes with the exchangeable cations [25].

# 3.7. Rotational viscosity test on the zeolite modified asphalt cement

The result of monitoring the viscosity of AC and ZA-AC samples after heating at 120  $^{\circ}$ C is presented in Table 4. For AC sample, over the first 60 min the viscosity keeps practically constant, therefore no significant changes are observed.

Compared to the non-modified asphalt cement, the ZA-AC sample (containing zeolite) present a higher viscosity, what is expected as a mineral was used as additive. However, when the ZA-AC sample is heated, a reduction in viscosity is observed within the first 20 min. Such

#### Table 4

Viscosity as a function of time for non-modified asphalt cement (AC) and zeolite modified asphalt cement (ZA-AC), at 120  $^\circ\text{C}.$ 

Time/min	Absolut viscosity/cP		Percentual viscosity/%		
	ZA-AC	AC	ZA-AC	AC	
0.5	887.5	855.0	100	100	
1.0	882.5	850.0	99.4	99.7	
6.0	865.0	850.0	97.4	99.4	
11	860.0	850.0	96.9	99.4	
16	860.0	852.5	96.9	99.7	
21	857.5	850.0	96.6	99.4	
26	852.5	847.5	96.0	99.1	
31	852.5	845.0	96.0	98.8	

a phenomenon results from the release of water present in the zeolite pores, promoting the micro foaming of the binder and consequently reducing its viscosity and enhancing its workability.

# 4. Conclusions

In summary, in this paper we have performed a series of different treatments to coal fly ash and applied them to the synthesis of zeolite A, in a high yield process that resulted in a distinguished material. Some aspects of the obtained zeolites showed to be influenced by the type of treatment employed to the fly ash. A novel pore characterization method, based on  $CO_2$  isotherms at 273 K and molecular simulation, revealed that almost all supercages of the synthetized sample ZA are unflawed.

The use of an important industrial by-product for the synthesis of zeolite A with minimum amounts of secondary phases, can dramatically reduce the zeolite production costs, allowing it to be applied in large scale applications such as its use as additive for warm mix asphalt, as demonstrated herein. The performance of the zeolite A, obtained from fly ash, in reducing the viscosity of asphalt cement makes it suitable for this purpose. Hopefully, the double environmental benefit related to the conversion of a waste into a product with high value-added and the considerable energy savings through the viability of WMA processes can drive the adoption of these technologies.



Fig. 6. Thermogravimetric and DSC analysis of sample ZA.

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### CRediT authorship contribution statement

Bruno C. Amoni: Conceptualization, syntheses, Data curation, Formal analysis, Investigation, Writing - original draft, Writing - review & editing. Armando D.L. Freitas: Conceptualization, syntheses, Data curation, Formal analysis, Investigation, Writing - original draft, Writing - review & editing. Raquel A. Bessa: Syntheses, Data curation, Formal analysis, Investigation, Writing - original draft, Writing - review & editing. Cristiane P. Oliveira: Formal analysis, Writing - original draft, Writing - review & editing. Moisés Bastos-Neto: CO2 isotherms acquisition, Data curation, Formal analysis, Investigation, Writing original draft, Writing - review & editing. Diana C.S. Azevedo: CO2 isotherms acquisition, Data curation, Formal analysis, Investigation, Writing - original draft, Writing - review & editing. José M. Sasaki: Data curation, Funding acquisition, Resources, Investigation, Writing original draft, Writing - review & editing. Jorge B. Soares: Conceptualization, Data curation, Funding acquisition, Resources, Investigation, Writing - original draft, Writing - review & editing. Sandra A. Soares: Conceptualization, Data curation, Funding acquisition, Resources, Investigation, Writing - original draft, Writing - review & editing. Adonay R. Loiola: Conceptualization, Data curation, Funding acquisition, Resources, Supervision, Investigation, Project administration, Writing - original draft, Writing - review & editing.

### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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#### Appendix A. Supplementary data

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